



PMME 2016

Thermal Conductivity and Impact Properties of Iron Ore Tailings Filled Epoxy Composites^{*}

M. A. Onitiri^{*}, E. T. Akinlabi

Department of Mechanical Engineering Science, University of Johannesburg, Auckland Park Kingsway Campus, 2006, South Africa

Abstract

Iron ore tailings which is the waste material derived from the beneficiation of iron ore was dispersed in epoxy as micro scale particle fillers. The effect of particle size and particle loading on the thermal conductivity and impact properties of the composites were then investigated experimentally. It was discovered that the impact resistance increased with increasing volume content of iron ore tailings from 20 vol. % with a maximum toughness of 0.098 kJm⁻² recorded for composite with 300 μm at 30 vol. %. Thermal conductivity of epoxy improved with decreasing particle size while 150 μm inclusion lead to improved thermal conductivity with increased volume content of filler.

© 2016 Elsevier Ltd. All rights reserved.

Selection and Peer-review under responsibility of International Conference on Processing of Materials, Minerals and Energy (July 29th – 30th) 2016, Ongole, Andhra Pradesh, India.

Keywords: Composites; Epoxy; Impact; Iron ore tailings; Particle size; Particle loading; Thermal conductivity

1. Introduction

Most modern design requires material with unusual combination of properties that cannot be met by conventional metals, metal alloys, ceramics and polymeric materials. The rapid increase in global population has led to corresponding increase in the consumption and exploration of this conventional materials with its negative environmental implications [1,2]. Composite materials have, over the years, been adopted to address the above

^{*} This is an open-access article distributed under the terms of the Creative Commons Attribution-NonCommercial-ShareAlike License, which permits non-commercial use, distribution, and reproduction in any medium, provided the original author and source are credited.

^{*} Corresponding author. Tel.: +2-778-044-9153; +2-761-495-1461.

E-mail address: monitiri@uj.ac.za

issues [3-7]. In the case of polymer, [3,7-9] inorganic particles such as micro-/nano- SiO_2 , Al_2O_3 , CaCO_3 , glass and carbon nanotubes are often added to improve their limitations (namely; low rigidity, low stiffness, low hardness, poor thermal and poor electrical conductivity) and to expand its application in different areas. Properties of the polymer matrix composites with particle inclusions are influenced by the particle size, the particle loading, the particle/matrix interfacial adhesion and the manufacturing processes [9,10]. This work intends to determine, experimentally, the effect of particle size and particle loading on the impact and thermal conductivity properties of iron ore tailings filled epoxy composites while the experimental thermal conductivity results will be compared to results obtained from existing theoretical models.

The use of metallic and non-metallic particles as fillers in polymers relates chiefly to applications requiring a certain degree of rigidity, hardness, toughness, abrasion, electrical conductivity, magnetic permeability, sound absorption and thermal conductivity. Non-metallic particle filled polymer composites find applications as structural materials in construction, packaging, automobile tyres, medicine, etc. while metal particle filled polymer composites are used in applications such as discharging static electricity, heat conduction (e.g. heat spreaders in notebook computers), electrical heating and communications. Previous works shows that stiffness and strength of particulate-filled polymer composites can be improved by addition of either micro- or nano-particle [9,11-13]. This is possible due to the higher stiffness property of the fillers compared to the polymer matrices while strength is improved by enhanced bonding between the particles and the matrices culminating to easy stress transfer between the particle and the matrices [9,14-17]. It has also been discovered that for applications which require high thermal conductivity, polymers which has lower thermal conductivity than those for metals or ceramic metals, exhibit improved thermal conductivity when organic or inorganic materials are added as fillers [18-21].

Adedayo and Onitiri's [22] work on the impact behaviour of iron ore tailings filled-polypropylene composites shows that Izod impact strength decreases with particle size but increases with increasing volume content of iron ore tailings from 5% to 25% for each particle size considered. In another work by Teh et al. [23] on the effect of particulate fused silica, glass powder and mineral silica on the thermal and the dynamic mechanical properties of epoxy composites, it was found that dynamic thermal mechanical properties and coefficient of thermal expansion (CTE) increase and reduce, respectively, with increasing volume of fillers. The highest toughness was observed at filler content 40 vol. %. In a related work, Zhang et al. [24] conducted thermal conductivity, impact and tensile tests on Al_2O_3 /high density polyethylene (HDPE) composites and found that thermal conductivity and tensile strength of the composites increased with decrease in particle size. Highest impact strength was exhibited by HDPE filled with 0.5 μm particle size Al_2O_3 at 25 vol. % content while nano-size particulate fillers lead to reduction in impact strength due to agglomeration of the particles caused by their high surface energy.

2. Materials and Experimentation

The epoxy resin is produced by Adefolorunsho Technical enterprises, Nigeria, under the brand name 'virgin epoxy'®. The epoxy resin was formed by reacting epichlorohydrin with bisphenol A. The particulate filler for this investigation is iron ore tailings from iron ore beneficiation plant in Itakpe, Kogi State in the North central region of Nigeria. It is approximately irregular in shape.

2.1. Iron ore tailings preparation

The iron ore tailings was dried at room temperature $30\pm 2^\circ\text{C}$ for a minimum of 40 hours prior to testing [25-27] while the different particle sizes were generated using standard ASTM laboratory sieves [28,29]. The uppermost of the ASTM sieve arrangement was loaded with iron ore tailings and vibrated for about 6 minutes. After vibrating, the sieve arrangement was dismantled and the tailings deposited in each sieve were weighed and recorded. The volume mix ratios adopted in this work are 0 to 30 % at intervals of 5 % while the particle sizes are 150, 212 and 300 μm .

2.2. Production of iron ore tailings filled epoxy composite test specimens

The dimensions of the impact and thermal conductivity test specimens are in conformity with ASTM D 256 – 10 and ASTM D 5930 – 09 specimen specifications, respectively [30,31]. The method used by Adedayo and Onitiri [32] was adopted for the production of the iron ore tailings filled epoxy composites. One and three parts of epichlorohydrin (hardener) and epoxy, respectively, were poured into a clean plastic container and stirred thoroughly with a wooden rod. Appropriate quantity of iron ore tailings was then added and stirred thoroughly so as to obtain a perfect mix and remove air. The poly (vinyl chloride) (PVC) film was fixed between the wooden base and the cavity strip. Then the mix was then poured and another PVC film was placed on the filled cavity followed by the wooden top. The arrangement was then clamped using the two threaded bolt and locking nut. The cast was allowed to cure for 80 minutes before the rig was dismantled and the cast removed. This procedure was carried out for different particle sizes and corresponding volume content of iron ore tailings. Five specimens were produced for each mix ratio.

2.3. Impact and thermal conductivity test

The Izod impact and thermal conductivity tests were conducted on the composites produced under standard laboratory atmosphere [23,24]. The test specimens were conditioned at room temperature $30^{\circ}\text{C} \pm 2^{\circ}\text{C}$ for a minimum of 40 hours prior to testing [25-27]. Conditioning was carried out to obtain reproducible results [25]. The Izod impact test was conducted as specified in ASTM D 256 – 10 using an Avery impact testing machine of capacity 4.2J and striking velocity 2.44m/s. The transient line-source technique was used for thermal conductivity test on the iron ore tailings [33] and the composites [31] using the KD2 Pro meter kit produced by Decagon Devices Inc.

3. Results and discussion

Fig. 1 shows the Izod impact toughness of iron ore tailings filled epoxy composites against 150, 212 and 300 μm particle size volume fraction content of 0-30 % vol. iron ore tailings at intervals of 5 % vol. particle inclusion. It can be seen that, though addition of iron ore tailings reduces the impact toughness of epoxy resin, the impact property of the composite improved with increased particle inclusion from 1.83 and 1.62 kJ/m^2 at 15 % to 2.32 and 2.25 kJ/m^2 at 30 % for 150 and 212 μm , respectively. 300 μm exhibited the highest impact strength from 15 % to 30 % with a value of 2.74 kJ/m^2 . It is significant to note that the 20 and 30 vol. % point, for low particle size inclusion, where epoxy composites exhibited approximately equal Izod impact toughness at variations of 0.05 and 0.07 kJ/m^2 , respectively. Liu et al. [34] also noted the significance of the 20 and 30 vol. % in their work on the effect of CaCO_3 ($d_p = 0.6 \mu\text{m}$) volume fraction on the Izod impact toughness of CaCO_3 filled high density polypropylene composites with various weight ratio of coupling agent. The Izod impact toughness for the composites peaked at 20 vol. % while poor toughening was shown at 30 vol. %. The Izod impact toughness is also found to increase with decreasing particle size in the particle volume fraction range studied. This is similar to findings reported by Bartczak et al. [35] and Zhang et al. [36] for CaCO_3 filled polymer composite under Izod impact loading. The former worked with polyethylene while the later used polypropylene matrices.

Fig. 2 shows the thermal conductivity versus volume of 150, 212 and 300 μm iron ore tailings in epoxy. It is observed that the thermal conductivity of epoxy improved with reducing particle size; with the highest value of 0.35 W/m-K recorded for 30 vol. % inclusion of 150 μm particle size fillers. It can also be seen that the thermal conductivity increases with increasing particle inclusion except for particle size 300 μm where the reverse is the case. The increase in thermal conductivity for the smaller particle sizes could be attributed to the improved particle compaction culminating into better surface area contact. On the other hand, reduction in thermal conductivity for 300 μm is due to the large particle size which leads to reduced surface area of particle contacting each other.

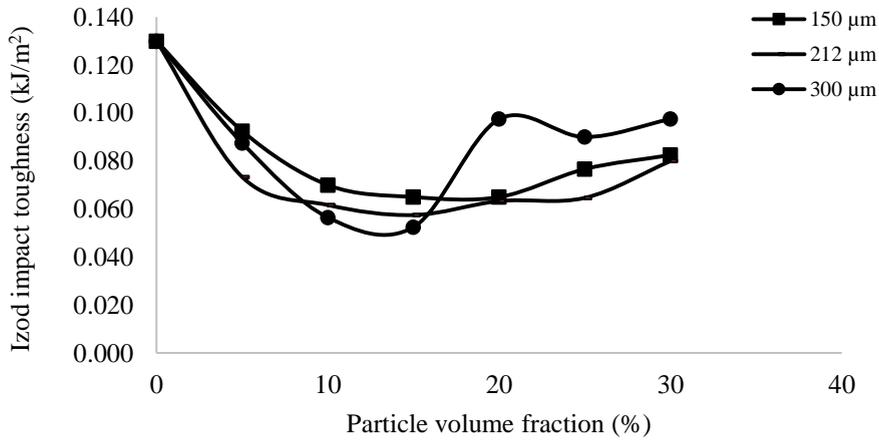


Figure 1: Notch Izod impact toughness of iron ore tailings filled epoxy composites versus iron ore tailings particle content

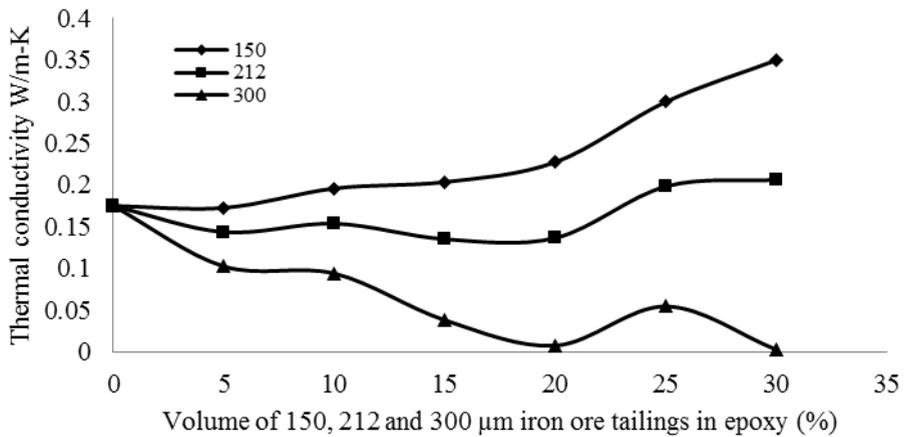


Figure 2: Thermal conductivity versus volume of 150, 212 and 300 μm iron ore tailings in epoxy

4. Conclusion

Impact strength of the composites with small particle sizes increased from 20 to 30 vol. % after the initial drop at lower % volume while composites with 300 μm inclusions exhibited the greatest impact resistance at volumes greater than 16.5 %. The thermal conductivity of epoxy improved with reduced particle size and increasing volume content for 150 and 212 μm particle fillers.

5. References

- [1] M.A. Onitiri, [dissertation], University of Ilorin, 2002.
- [2] M.A. Onitiri, J.S.O. Adeniyi, *Nigerian J. Techn. Develop.* 3 (2003) 80-87.
- [3] S.N. Maiti, P.K. Mahapatro, *J. Appl. Polym. Sci.* 42 (2011) 3077-3273.
- [4] R. Rahman, M. Hasan, M. Huque, *J. Thermoplas. Comp. Mat.* 22 (2009) 365-381.
- [5] R. Rahman, M. Huque, N. Islam, *Compo. Part A.* 40 (2009) 511-517.
- [6] G.V. Reddy, S.V. Naidu, T.S. Rani, *J. Reinf. Plast. Compos.* 28 (2009) 2035-2044.
- [7] K. Chandrakala, A. Vanaja, R. Rao, *J. Reinf. Plast. Compos.* 28 (2009) 1987-1997.
- [8] J. Wang, [dissertation]. Austin (US): The University of Texas at Austin; 2003.
- [9] S. Fu, X. Feng, B. Lauke, *Compo. Part B: Engineering.* 39 (2008) 933-961.
- [10] M.A. Onitiri, S.M. Adedayo, *J. Eng. Design Techn.* 13 (2015) 198-212.
- [11] Z.K. Zhu, Y. Yang, J. Yin, *J. Appl. Polym. Sci.* 73 (1999) 2977-2984.
- [12] K.C. Radford, *J. Mater. Sci.* 6 (1971) 1286–91.
- [13] N. Amdouni, H. Sautereau, J.F. Gerard, *J. Appl. Polym. Sci.* 46 (1992) 1723–35.
- [14] C.H. Hsueh, *J. Am. Ceram. Soc.* 72 (1987) 344–7.
- [15] B. Pukánszky, G. Voros, *Compos. Interf.* 1 (1993) 411-427.
- [16] R.J. Young, P.W.R. Beaumont, *J. Mat Sci.* 12 (1978) 643-657.
- [17] Y. Nakamura, M. Yamaguchi, M. Okubo, *J. Appl. Polym. Sci.* 45 (1992) 1281-1289.
- [18] D. Kumlutas, I.H. Tavman, M.T. Coban, *Compos. Sci. Techn.* 63 (2003) 113– 117.
- [19] H. Ishida, U.S. Patent 5,900,447. (1999).
- [20] H. Ishida, U.S. Patent 6,160,042. (2000).
- [21] H. Ebadi-Dehaghani, M. Nazempour, in: A. Hashim (Eds.), *Thermal conductivity of nanoparticles filled polymers*, InTech, Rijeka, 2012, pp. 519–540.
- [22] S.M. Adedayo, M.A. Onitiri, *J. Min. Mat. Charact. Eng.* 11 (2012) 671-678.
- [23] P.L. Teh, M. Jaafar, H.M. Akil, *Polym. Adv. Techn.* 19 (2008) 308-315.
- [24] S. Zhang, X.Y. Cao, Y.M. Ma, *eXPRESS Polym. Letter.* 5 (2011) 581–590.
- [25] ASTM D618-13, *Standard Practice for Conditioning Plastics for Testing*, West Conshohocken: ASTM International; 2013.
- [26] ASTM E171 / E171M-11(2015), *Standard Practice for Conditioning and Testing Flexible Barrier Packaging*. West Conshohocken: ASTM International; 2015.
- [27] ASTM E41-92 (2010), *Terminology Relating to Conditioning*. West Conshohocken: ASTM International; 2010.
- [28] S. O. Adepoju, B.M. Olaleye, *Nig. J. Eng. Man.* 2 (2001) 51-55.
- [29] P. A. Olubambi, J.H. Potgieter, *J. Min. Mat. Charact. Eng.* 4 (2005) 21-30.
- [30] ASTM D256-10e1, *Standard Test Methods for Determining the Izod Pendulum Impact Resistance of Plastics*. West Conshohocken: ASTM International; 2010.
- [31] ASTM D5930-09, *Standard Test Method for Thermal Conductivity of Plastics by Means of a Transient Line Source Technique*. West Conshohocken: ASTM International; 2009.
- [32] S.M. Adedayo, M.A. Onitiri, *The West Ind. J. Eng.* 35 (2012) 51-59.
- [33] ASTM D5334-08, *Standard Test Method for Determination of Thermal Conductivity of Soil and Soft Rock by Thermal Needle Probe Procedure*. West Conshohocken: ASTM International; 2008
- [34] Z.H. Liu, K.W. Kwok, R.K.Y. Li, *Polym.* 43 (2002) 2501–2506.
- [35] Z. Bartczak, A.S. Argon, R.E. Cohen, *Polym.* 40 (1999) 2347–2365.
- [36] L. Zhang, C. Li, R. Huang, *J. Polym. Sci. Part B: Polym. Phys.* 42 (2004) 1656–1662.